

IN THE DRAWINGS:

Please approve the change in the drawings as indicated in red on the photocopy being submitted simultaneously herewith together with another document entitled LETTER TO OFFICIAL DRAFTSPERSON. The amendment comprises changing "RUMP" to --RAMP-- at three places in Fig. 5.

IN THE SPECIFICATION:

Replace the paragraph starting at line 21 of page 1 with the following rewritten paragraph:

Fig. 5 shows an example of a general temperature program set for a prior art atomic absorption spectrophotometer. Fig. 6 is a graph for showing the temperature variation according to the temperature program thus set. The example of the temperature program shown in Fig. 5 may be characterized as dividing the time into a plurality (six in the example shown) of stages and setting for each of these stages the final temperature to be reached, the time which will elapse until this final temperature is reached and the heating mode related to the temperature change. In the column for the heating mode in Fig. 5, RAMP means a mode in which the temperature is to increase uniformly, or linearly at a constant rate with respect to time and "step" means a mode in which the temperature increases suddenly in a stepwise fashion.

Replace the paragraph starting at line 22 of page 3 with the following rewritten paragraph:

As explained above, prior art spectrophotometers were designed to increase the temperature as rapidly as possible so as to shorten the time required to reach the target temperature without regard to the response characteristic such as the indicial response characteristic corresponding to the step response characteristic as the temperature is increased in a stepwise fashion. A furnace-type atomic absorption spectrophotometer according to this

invention, by contrast, is characterized wherein its temperature response characteristic is made variable as the increase in the temperature of the heating tube is controlled. As a result, the rise in the temperature can be controlled according to this invention by providing an optimum response characteristic, depending on the kind of the target element to be detected as well as other conditions of the measurement, such that the minimum detectable quantity can be made as small as possible. The response characteristic according to this invention is determined in units of milliseconds, unlike the prior art "ramp" mode of temperature control which takes place in units of seconds.

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Replace the paragraph starting at line 6 of page 4 with the following rewritten paragraph:

A furnace-type atomic absorption spectrophotometer embodying this invention, with which the above and other objects can be accomplished, may be characterized as comprising a tube for heating a sample therein, monitoring means for monitoring temperature of the tube or a value indicative thereof and outputting a monitored temperature or the value indicative thereof, heating control means for controlling an electrical heating current for heating the tube such that the monitored temperature or the value indicative thereof will approach a specified target temperature value, and parameter setting means for setting parameters which determine a response characteristic of the heating control means when the tube is heated by the heating control means. The monitoring means may be an optical detector for detecting the light emitted from the tube and in such a case the value indicative of the temperature may be the intensity of the emitted light. The heating control means serves to keep updating the target temperature value or another variable value indicative of the target temperature by a predetermined temperature program and controls the heating current to the tube such that the monitored value obtained by the monitoring means will become or approach this target temperature or the value indicative thereof. Generally speaking, the heating current is increased if the difference between the target temperature and the monitored temperature is large and it is decreased if the difference

is small. The response characteristic associated with this control is variable according to the parameters which are set by the parameter setting means. In typical examples, these parameters are appropriately adjusted according to the kind of target element being analyzed. The magnitude of absorbance depends differently on the speed at which temperature is raised, depending on the type of the elements. In the case of an element of which absorbance depends only weakly on the rate of temperature increase, parameters are selected such that the obtained response characteristic will be such that the speed in the temperature change will not become too large because the absorbance of such an element will become saturated or its increase will be extremely small when the rate of temperature increase is made greater than a certain level. If various modifiers have been added to the sample, the parameters should be changed appropriately by taking into consideration the characteristics of these added agents.

Replace the paragraph starting at line 27 of page 5 with the following rewritten paragraph:

The heating control means according to this invention may be adapted to carry out a PID control calculation on the difference between the monitored and target values to obtain a quantity of specified operation. Since the quantity of the specified operation is determined by this control method from the proportional (P), integration (I) and differential (D) operations based on the difference between the monitored and target values, proportional, integration and differential elements serve as the aforementioned control parameters. If the electric current for the heating is switched on and off by a phase control method, the firing angle for the phase control may be the aforementioned quantity of a specified operation.

Replace the paragraph starting at line 18 of page 8 with the following rewritten paragraph:

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Next, the operations for the temperature control of the graphite tube 3 are explained. At the beginning of a measurement, the user inputs through the keyboard 25 a temperature program such as shown in Fig. 5. The inputted temperature program is then stored in the temperature setting means 24 which already stores a target value for the optical sensor 16 corresponding to the temperature. As the graphite tube 3 is heated, the output from the optical sensor 16 corresponding to the measured temperature is inputted as a digital signal into the calculator 21 by going through the A/D converter 18. At the same time, a target value for the optical sensor 16 corresponding to the set temperature at the present time is provided from the temperature setting means 24 to the calculator 21. The calculator 21 operates to calculate the difference between the current output value from the optical sensor 16 and the target value and calculates the firing angle  $\alpha$  by using a calculation algorithm for the PID control on the basis of this difference value. The pulse generator 19 thereupon produces a pulse signal corresponding to this firing angle  $\alpha$  and carries out the on/off control of the semiconductor switch 11.

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Replace the paragraph starting at line 3 of page 9 with the following rewritten paragraph:

For carrying out the aforementioned PID control, it is necessary to provide so-called PID control parameters including the proportional parameter P, integration parameter I and differential parameter D. If these parameters are changed, the temperature response characteristic will change at the time of rise in the temperature. Let us consider an example of control wherein the outputs from the optical sensor 16 are monitored at a sampling period of  $T_s$  and the outputted values are controlled so as to become stabilized at a value corresponding to the target temperature by appropriately adjusting the firing angle  $\alpha$  which determines the power for heating the tube 3 according to these monitored values. Let  $E_k$  be the error obtained by subtracting the monitored value from the target value at the time of the  $k$ th sampling ( $k$  being a dummy index). Then, the firing angle  $\alpha_k$  is given by the following formula:

$$\alpha_k = K_p \{ E_k + (T_s/T_i) \sum_{j=0}^k E_j + (T_d/T_s) (E_k - E_{k-1}) \}$$

*Q6*  
where  $K_p$ ,  $T_i$  and  $T_d$  are PID control parameters to be set, being respectively referred to as the proportional gain, the integration time and the differentiation time.

Replace the paragraph starting at line 16 of page 12 with the following rewritten

paragraph:

*a>*  
Although the invention has been described above with reference to only one example, this example is not intended to limit the scope of the invention. Many modifications and variations are possible within the scope of the invention. For example, although it was shown that the PID control parameters are to be inputted by the user, control parameters which will minimize the minimum detectable quantity under several different conditions of measurement may be preliminarily stored such that the user has only to input conditions of measurement from the keyboard 25 such that appropriate control parameters are automatically selected and inputted to the calculator 21.

Replace the paragraph starting at line 24 of page 12 with the following rewritten paragraph:

*q8*  
The control unit 20 may be also designed so that PID control parameters will be automatically set so as to minimize the minimum detectable quantity or make it approach such a minimum value under a given condition. Explained more in detail, this may be done when a measurement is to be made on a certain sample under a certain condition by repeating measurements with a set of PID control parameters while varying them and thereby obtaining an average absorbance value and its standard variation and finding PID control parameters that will